

1 **Transient climate response in a two-box energy-balance model.**

2 **Part II: representation of the efficacy of deep-ocean heat uptake**

3 **and validation for CMIP5 AOGCMs.**

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ABSTRACT

7
8 In this second part of a series of two articles analyzing the global thermal properties of
9 atmosphere-ocean coupled General Circulation Models (AOGCMs) within the framework of
10 a two-box Energy Balance Model (EBM), the role of the efficacy of deep-ocean heat uptake is
11 investigated. Taking into account such an efficacy factor is shown to amount to representing
12 the effect of deep-ocean heat uptake on the local strength of the radiative feedback in the
13 transient regime. It involves an additional term in the formulation of the radiative imbalance
14 at Top-of-the-Atmosphere (TOA) that explains the nonlinearity between radiative imbalance
15 and mean surface temperature observed in some AOGCMs. An analytical solution of this
16 system is given and this simple linear EBM is calibrated for the set of 12 CMIP5 AOGCMs
17 studied in Part I. It is shown that both net radiative fluxes at TOA and global surface
18 temperature transient response are well represented by the simple EBM over the available
19 period of simulations. Differences between this two-box EBM and the previous version
20 without efficacy factor are analyzed and relationships between parameters are discussed.
21 The simple model calibration applied to AOGCMs constitutes a new method for estimating
22 their respective equilibrium climate sensitivity and adjusted radiative forcing amplitude from
23 short-term step-forcing simulations and more generally a method to compute their global
24 thermal properties.

1. Introduction

In Part I (Geoffroy et al. 2012, hereafter G12), it is shown using the CMIP5 database that a two-box energy-balance model calibrated only from an AOGCM step-forcing experiment is able to reproduce gradual CO₂-increase idealized scenarios. Such a calibration gives the first-order global thermal properties characterizing an AOGCM. The calibration method requires to determine both the reference radiative forcing amplitude and the equilibrium climate sensitivity (ECS), defined as the equilibrium mean surface temperature response for a 2xCO₂ radiative perturbation.

Determining the amplitude of the radiative forcing associated with a given externally-imposed perturbation, and the ECS remain an issue and a topic of debate in the literature [e.g. Knutti and Hegerl (2008)]. While the evaluation of the radiative forcing is complicated by the existence of fast stratospheric and tropospheric adjustments (Gregory and Webb 2008), the determination of the ECS requires very long simulations (thousands of years) and is computationally expensive. Alternative methods have been proposed for estimating the equilibrium climate sensitivity. For example, it can be evaluated by coupling the atmospheric general circulation model (AGCM) to a mixed-layer ocean (ML). However, on the one hand, such an estimation remains computationally expensive. On the other hand, an AOGCM and its AGCM-ML counterparts estimates of the ECS may differ because the ocean circulation redistributes the energy and impacts the Earth’s energy balance through its interaction with atmospheric processes.

Another type of methods consists in extrapolating the transient regime AOGCMs response to equilibrium. These methods lie on the linear assumption between the TOA radiative imbalance N and the mean surface temperature response: $N = \mathcal{F} - \lambda T$. Murphy (1995) introduced the effective climate sensitivity such that it can be deduced from the non-balanced mean surface temperature response and the amplitude of the radiative imbalance: $ECS/T(t) = \mathcal{F}_{2xCO_2}/(\mathcal{F}_{2xCO_2} - N(t))$. But this estimation requires the knowledge of the radiative forcing \mathcal{F}_{2xCO_2} that must be deduced by an independent method. Gregory et al.

52 (2004) refined the estimate of the effective ECS by fitting the net radiative flux at TOA as a
53 function of T along the whole period of an abrupt $2\times\text{CO}_2$ or a stabilization scenario. This in-
54 troduces the concept of effective forcing. Such a fit gives the effective forcing (intercept), the
55 effective radiative feedback parameter (slope) and the effective equilibrium climate sensitiv-
56 ity (x-axis intersection). The estimated forcing takes into account all the fast (few months)
57 feedbacks that cannot be considered as feedbacks associated with the surface temperature
58 response, such as stratospheric and tropospheric adjustments (Gregory and Webb 2008).

59 The main shortcoming of this type of methods is that the ECS is found to vary in time
60 for some models and methods (Gregory et al. 2004; Senior and Mitchell 2000; Boer and Yu
61 2003b). This questions the validity of the linear assumption between N and T that is in the
62 heart of energy-balance models (EBMs). Williams et al. (2008) showed that a bias in the
63 estimation of the radiative forcing is partly responsible for these variations but not totally;
64 the assumption of linearity itself has limitations. Indeed, one needs to distinguish between
65 the temperature response induced by radiative flux for a given equilibrium temperature
66 amplitude (i.e. a given radiative forcing) and for a given temperature amplitude in transient
67 regime. Whereas the linear dependency assumption is reasonably robust in the first case, it
68 is found not to be valid in the second case, at least for some climate models (Gregory et al.
69 2004; Williams et al. 2008; Winton et al. 2010).

70 Using CMIP3 idealized scenario simulations, Winton et al. (2010) showed that an addi-
71 tional process needs to be taken into account during the transient regime in order to represent
72 the evolution of the radiative imbalance of the climate system. The ocean heat uptake re-
73 duces the rate of warming and this effect occurs preferentially in some regions, specially
74 those corresponding to the sinking branches of the thermohaline circulation, in the North
75 Atlantic ocean and circumpolar ocean of the southern hemisphere (Manabe et al. 1991).
76 This modifies the transient regime temperature pattern in comparison with the equilibrium
77 pattern. Because the feedback strength varies geographically, the pattern of surface temper-
78 ature changes induced by the ocean heat uptake may impact the radiative imbalance in the

79 transient regime. This reasoning led Winton et al. (2010) to introduce an efficacy factor for
80 the ocean heat uptake. Held et al. (2010) introduced such an efficacy factor in the two-box
81 linear EBM.

82 In this study, this simple model is used to determine the ECS, the adjusted radiative
83 forcing and the thermal inertia properties of a given AOGCM by taking into account the
84 effect of deep-ocean heat uptake on the radiative imbalance during the transient regime.
85 This allows to compute all the parameters consistently in a single framework. In Section 2,
86 the model with this feature is presented, underlying assumptions of the model are discussed
87 and the calibration method is described. In Section 3, this method is applied to CMIP5
88 abrupt 4xCO₂ experiments. Results are discussed and compared to results obtained with
89 the previous version of the EBM, without efficacy factor. The existence of relationships
90 between the parameters is then investigated. Finally, a decomposition of the TOA net
91 radiative flux in longwave and shortwave components is performed within the framework of
92 this simple model.

93 **2. Two-box model with an efficacy factor for deep-ocean** 94 **heat uptake**

95 *a. System of equations and analytical solution*

96 In this Part II, we consider the following two-box EBM with an efficacy factor for deep-
97 ocean heat uptake ε proposed by Held et al. (2010):

$$C \frac{dT}{dt} = \mathcal{F} - \lambda T - \varepsilon \gamma (T - T_0), \quad (1)$$

$$C_0 \frac{dT_0}{dt} = \gamma (T - T_0), \quad (2)$$

98 where C , C_0 and γ are respectively the first-layer (atmosphere/land/upper-ocean) surfacic
99 heat capacity, the second-layer (deep-ocean) surfacic heat capacity and the heat exchange

100 coefficient between the two layers. The term $\gamma(T - T_0)$ is the heat flux H exchanged between
 101 the two layers and is equal to the deep-ocean heat uptake: $H = \gamma(T - T_0)$. Since the change
 102 in the heat content of the first layer CdT/dt is driven by the sum of the heat flux exchanged
 103 with the deep ocean $-H$ and the heat flux exchanged with the external system N , the net
 104 radiative flux at TOA evolves as:

$$N = \mathcal{F} - \lambda T - (\varepsilon - 1)H. \quad (3)$$

105 In the following, EBM-1 will refer to the standard energy-balance model analyzed in G12
 106 and EBM- ε to the model described above. The presence of an additional radiative flux term,
 107 $(\varepsilon - 1)H$, in the evolution of N constitutes the main difference with the EBM-1. In the case
 108 of a gradual increase of the external perturbation, CdT/dt is small (see G12); in the limit
 109 of negligible CdT/dt , $N = H$ and Eq. (3) leads to the formulation of Winton et al. (2010)
 110 [see their Eq. (3)]:

$$T_{eq} - T = \frac{\varepsilon}{\lambda}N, \quad (4)$$

111 with the equilibrium temperature response defined as $T_{eq} = \mathcal{F}/\lambda$.

112 By introducing $C'_0 = \varepsilon C_0$ and $\gamma' = \varepsilon\gamma$, the system can be written as follows:

$$C \frac{dT}{dt} = \mathcal{F} - \lambda T - \gamma'(T - T_0), \quad (5)$$

$$C'_0 \frac{dT_0}{dt} = \gamma'(T - T_0), \quad (6)$$

113 which is the same mathematical system as that of the EBM-1 except for the primes. As
 114 pointed by Held et al. (2010), the effect of the deep-ocean efficacy factor is equivalent to
 115 modifying ocean properties such that its surfacic heat capacity and the heat exchange coef-
 116 ficient between the two layers are scaled by a factor ε . Note that the EBM- ε is physically
 117 different from the EBM-1 because it includes an additional process. As a result, all the phys-
 118 ical parameters estimated on the basis of this model can be different from their counterparts
 119 estimated within the framework of the EBM-1. The derivation of the analytical solution
 120 of the EBM- ε is straightforward. All the formulations of the eigenmode parameters given

121 in G12 are still valid by replacing C_0 (respectively, γ) by C'_0 (resp., γ'). These parameters
 122 are noted with the primes in the following. For a step forcing and a linear forcing with an
 123 increase rate F , the mean surface temperature response is, respectively:

$$T(t) = \frac{\mathcal{F}}{\lambda} - \frac{\mathcal{F}}{\lambda} a'_f e^{-t/\tau'_f} + \frac{\mathcal{F}}{\lambda} a'_s e^{-t/\tau'_s}, \quad (7)$$

$$T(t) = \frac{F}{\lambda} t - \frac{F}{\lambda} \tau'_f a'_f (1 - e^{-t/\tau'_f}) - \frac{F}{\lambda} \tau'_s a'_s (1 - e^{-t/\tau'_s}), \quad (8)$$

124 where τ'_f , a'_f , τ'_s and a'_s are the fast and slow eigenmode parameters defined in G12 and
 125 expressed as functions of λ , C , C'_0 and γ' .

126 *b. EBM- ε underlying hypothesis*

127 1) GLOBAL BUDGET

128 In this section, the hypothesis underlying the introduction of an efficacy factor ε are
 129 presented. Within the framework of a two-layer simple climate model, the change in the heat
 130 content of the climate system is the sum of the atmosphere/land/upper-ocean instantaneous
 131 heat uptake CdT/dt and the deep-ocean instantaneous heat uptake C_0dT_0/dt . This change
 132 is equal to the net radiative imbalance N at the top of the atmosphere:

$$C \frac{dT}{dt} + C_0 \frac{dT_0}{dt} = N. \quad (9)$$

133 Thus N can be decomposed into two radiative contributions N_U and N_D equal to the in-
 134 stantaneous rate of heat storage respectively in the upper and the deep oceans. Similarly,
 135 the temperature associated with the heat-uptake $T_H = T - T_{eq}$ (Winton et al. 2010; Ge-
 136 offroy et al. 2012) can be decomposed into the sum of an upper-ocean contribution and a
 137 deep-ocean contribution: $T_H = T_U + T_D$. It is then assumed that the contributions to the
 138 TOA radiative imbalance induced by upper- and deep-ocean heat uptakes N_U and N_D are
 139 linear functions, respectively, of T_U with a feedback parameter λ and of T_D with a feedback

140 parameter λ_D :

$$C \frac{dT}{dt} = N_U = -\lambda T_U, \quad (10)$$

$$C_0 \frac{dT_0}{dt} = H = N_D = -\lambda_D T_D. \quad (11)$$

141 The deep-ocean heat-uptake temperature is associated with a different feedback parameter
 142 λ_D because the spatial pattern of the deep-ocean heat-uptake temperature differs from the
 143 equilibrium surface temperature response pattern. Following Hansen et al. (2005), Held et al.
 144 (2010) and Winton et al. (2010), an efficacy factor for deep-ocean heat uptake is introduced:

$$\varepsilon = \lambda/\lambda_D. \quad (12)$$

145 Summing Eqs. (10) and (11) leads to:

$$C \frac{dT}{dt} + H = -\lambda T_U - \frac{\lambda}{\varepsilon} T_D. \quad (13)$$

146 By using $T - T_{eq} = T_U + T_D$ and $H = -\lambda_D T_D$, Eq. (13) is equivalent to Eq. (1).

147 2) LOCAL BUDGET

148 To understand why the feedback strength may vary with the temperature pattern, it
 149 can be useful to examine the evolution of the local energy balance in transient regime. As
 150 pointed by Boer and Yu (2003a), the change in heat content of a climate system column is
 151 equal to the local radiative imbalance and the local convergence of the horizontal energy:

$$\frac{dh^i}{dt} + \frac{dh_0^i}{dt} = \mathcal{F}^i - \lambda^i T^i + A_t^i + A_{0t}^i, \quad (14)$$

152 where dh^i/dt and dh_0^i/dt are the local change in the heat content respectively of the first
 153 and the second layer; T^i , \mathcal{F}^i and λ^i are respectively the local temperature response, the
 154 local forcing and the local feedback parameter; A_t^i and A_{0t}^i are the local convergence of the
 155 horizontal energy flux respectively of the first and the second layer. The superscript "i"
 156 denotes local values. The average over the Earth's surface of dh^i/dt (respectively, dh_0^i/dt)

157 is the change in the heat content of the first layer CdT/dt (respectively, of the second layer
 158 $C_0dT_0/dt = H$). The global mean of the local forcing is \mathcal{F} . The global average of each local
 159 energy convergence A_t^i and A_{0t}^i is 0. Note that the local heat flux from the upper ocean to
 160 the deep ocean H^i verifies:

$$\frac{dh_0^i}{dt} = H^i + A_{0t}^i. \quad (15)$$

161 Equation (14) can be viewed as the heat budget in response to the sum of three "forcings":
 162 the external forcing \mathcal{F}^i and two sink terms, the upper-ocean heat uptake dh^i/dt and the deep-
 163 ocean heat uptake dh_0^i/dt , being considered as "internal forcings". By assuming additivity
 164 of the temperature response patterns (Forster et al. 2000; Boer and Yu 2003a), the local
 165 surface temperature response can be expressed as the sum of the balance response to these
 166 "forcings": $T^i = T_{eq}^i + T_U^i + T_D^i$, and the local budget (14) can be decomposed in the following
 167 system of equations:

$$\mathcal{F}^i - \lambda^i T_{eq}^i + A_{eq}^i + A_{0eq}^i = 0, \quad (16)$$

$$-\frac{dh^i}{dt} - \lambda^i T_U^i + A_U^i + A_{0U}^i = 0, \quad (17)$$

$$-\frac{dh_0^i}{dt} - \lambda^i T_D^i + A_D^i + A_{0D}^i = 0, \quad (18)$$

168 where T_U^i and T_D^i are the local upper-ocean and deep-ocean heat-uptake temperatures, i.e.,
 169 the temperature responses to the upper-ocean and deep-ocean heat-uptake "forcings". A_{eq}^i ,
 170 A_U^i and A_D^i , are the associated convergences of horizontal energy fluxes in the first layer, with
 171 $A_t^i = A_{eq}^i + A_U^i + A_D^i$. Similarly, A_{0eq}^i , A_{0U}^i and A_{0D}^i are the convergences of horizontal energy
 172 fluxes in the second layer. Note that the global average of each energy-flux convergence A_x^i
 173 and A_{0x}^i is zero. Assuming that A_{0U}^i is 0 leads to $A_{0D}^i = A_{0t}^i - A_{0eq}^i$. Also, the decomposition
 174 of T and A_t in sums, Eq. (14) and Eqs. (16)-(18) leave one degree of freedom in the definition
 175 of T_U^i , T_D^i , A_U^i and A_D^i .

176 Introducing the normalized equilibrium temperature amplitude function $r_{eq}^i = T_{eq}^i/T_{eq}$,
 177 the local heat budget at equilibrium is:

$$\mathcal{F}^i - \lambda^i r_{eq}^i T_{eq} + A_{eq}^i + A_{0eq}^i = 0. \quad (19)$$

178 One can note that the equilibrium temperature pattern, i.e. r_{eq}^i , depends on the local
 179 forcing, the local feedback and the amplitude of the local energy convergence. Thus, the
 180 total feedback parameter λ is the average of the local feedback parameter weighted by the
 181 equilibrium temperature pattern:

$$\lambda = \frac{1}{S} \iint r_{eq}^i \lambda^i dS. \quad (20)$$

182 This parameter will be referred as the equilibrium feedback parameter in the following.

183 By assuming the separability of time and space variables for T_U^i and T_D^i , they can be
 184 decomposed in the product of a time-varying global average T_x by a spatial pattern r_x^i .
 185 On one hand, the upper-ocean heat content change has a relaxation time that is lower
 186 than the typical scale of interannual variability. We expect the pattern of T_U^i to be similar
 187 to the equilibrium pattern. By defining A_U^i such that $-dh^i/dt + A_U^i$ is the projection of
 188 $-dh^i/dt + A_t^i - A_{eq}^i$ onto the pattern $\lambda^i r_{eq}^i$, we can impose that the pattern of T_U^i is the same
 189 as that of the equilibrium temperature: $r_U^i = r_{eq}^i$. Note that this equality is imposed by the
 190 initial conditions in the case of a step forcing: $T_U(0) = -T_{eq}(0)$ and $T_U^i(0) = -T_{eq}^i(0)$. On
 191 the other hand, the pattern of T_D depends on the local deep-ocean heat uptake and on the
 192 residual energy convergences. Because the pattern of the deep-ocean heat uptake is different
 193 from the pattern of the radiative forcing, T_D^i is assumed to be associated with a pattern
 194 $r_D^i \neq r_{eq}^i$. Averaging Eq. (18) over the Earth's surface leads to Eq. (11) with the following
 195 formulation of λ_D :

$$\lambda_D = \frac{1}{S} \iint r_D^i \lambda^i dS. \quad (21)$$

196 The weight coefficient r_D^i is different from the one in the equilibrium feedback parameter
 197 expression. If the strength of the local feedback λ^i is low in regions where the ocean heat-
 198 uptake induces a small temperature increasing rate (resulting in high values of r_D^i), then λ_D
 199 is lower than λ . Consequently, for a given amplitude of T_U and T_D , N_D is smaller, i.e., the
 200 climate system accumulates less heat.

201 To conclude Section 2b, the introduction of an efficacy factor for the deep-ocean heat

202 uptake is the result of a decomposition of the temperature pattern as the sum of the temper-
 203 ature response patterns to the radiative forcing, the upper-ocean and the deep-ocean heat
 204 uptakes assuming a linear relationship between these "forcings" and their associated temper-
 205 ature responses. Because the spatial pattern of the temperature response to the deep-ocean
 206 heat uptake differs from the equilibrium pattern, the spatial heterogeneity of the radiative
 207 feedbacks strength involves that the magnitude of the global radiative feedback varies in
 208 time during a climate transition.

209 *c. Effect of efficacy factor of deep-ocean heat uptake*

210 In case of a step forcing, the analytical solutions for the upper-ocean and deep-ocean
 211 heat-uptake temperatures are:

$$T_U(t) = -\frac{\mathcal{F}}{\lambda} \left[f'_U a'_f e^{-t/\tau'_f} + s'_U a'_s e^{-t/\tau'_s} \right], \quad (22)$$

$$T_D(t) = -\frac{\mathcal{F}}{\lambda} \left[f'_D a'_f e^{-t/\tau'_f} + s'_D a'_s e^{-t/\tau'_s} \right]. \quad (23)$$

212 The expression, the order of magnitude and the sign of the fractional contributions a'_f , a'_s ,
 213 f'_U , f'_D , s'_U and s'_D are given in G12 (by replacing C_0 and γ by, respectively, C'_0 and γ' in the
 214 expressions).

215 The theoretical temporal evolutions of T , T_U and T_D in the case of a step-forcing are
 216 represented in the upper panels of Fig. 1 for three values of efficacy factor: $\varepsilon < 1$, $\varepsilon = 1$
 217 and $\varepsilon > 1$ and other parameters unchanged. The upper-ocean heat-uptake temperature T_U
 218 increases with the characteristic timescale τ'_f , and after few years, it tends to zero since the
 219 contribution s'_U of the slow mode to T_U is negligible: the upper-ocean reservoir is saturated.
 220 Concerning the deep-ocean heat-uptake temperature, the contributions of the slow and fast
 221 modes (s'_D and f'_D) are comparable but of opposite signs. The fast mode is predominant
 222 in the first few years and induces a decrease in T_D , i.e., the heat flux exchanged between
 223 the two layers H increases because T increases faster than T_0 . After this first phase (with
 224 a characteristic duration of τ'_f), the slow mode becomes dominant and T_D increases slowly

225 back to zero: the deep ocean accumulates less and less heat.

226 The middle panels of Fig. 1 represent the theoretical relationship between the radiative
227 imbalance N and the mean surface temperature perturbation T during the transient regime,
228 for the same values of ε . The intercept and the x-axis intersection are independent from the
229 value of ε . Per definition, the intercept at $T = 0$ is the amplitude of the forcing \mathcal{F} (Gregory
230 et al. 2004). Similarly, the x-axis intersection is the equilibrium temperature response (the
231 equilibrium climate sensitivity in the case of a $2\times\text{CO}_2$ perturbation per definition). Only the
232 path to join these two points is altered when ε is modified.

233 With $\varepsilon = 1$, the net radiative flux varies linearly with the temperature. For $\varepsilon \neq 1$, the
234 plots suggest that there are two distinct stages in the (N, T) response to an abrupt forcing.
235 To understand this behaviour, it is convenient to decompose the net flux into the sum of its
236 two components contribution N_U and N_D . In Fig. 1 (middle row), the evolutions of (N_U, T)
237 and (N_D, T) are plotted respectively with gray solid lines and dash-dotted lines.

238 During the first period, corresponding to the fast mode response timescale, the two com-
239 ponents (upper and deep oceans) contribute with a similar amplitude but with opposite
240 trends to the temperature response and N varies roughly linearly with T . Indeed, neglecting
241 the slow response term during this period, the time evolutions of N_U and N_D are proportion-
242 nal to that of T_H (and T); the scale factors are, respectively, $-\lambda f'_U$ and $-\lambda_D f'_D$, with $f'_U > 0$
243 and $f'_D < 0$. Accordingly, the radiative imbalance N as the sum of these two contributions
244 evolves roughly linearly with T .

245 During the second period, the contribution of the upper ocean is negligible ($s'_U \ll 1$) and
246 the net radiative flux is simply the contribution of the deep-ocean heat-uptake temperature:
247 $-\lambda_D T_D$. Then, since $T_D \approx T - T_{eq}$, the radiative flux varies also roughly linearly with T .
248 The sharp change in the trend of the (N, T) line corresponds to a time similar to the fast
249 relaxation time. This analysis suggests that linear fits of the two asymptots of the (N, T)
250 curve performed separately as in Gregory et al. (2004) give a good approximation of the
251 radiative forcing \mathcal{F} (as the intercept of the first fit), the equilibrium temperature T_{eq} (as the

252 x-axis intersection of the second fit), and $\lambda_D = \lambda/\varepsilon$ (as the slope of the second fit).

253 The net radiative flux at the top of the atmosphere can also be decomposed as the sum
254 of prognostic variables and physical parameters of the EBM- ε as shown in Eq. (3). The
255 radiative imbalance N is the sum of a linear term $\mathcal{F} - \lambda T$ and a fraction $1 - \varepsilon$ of the
256 instantaneous rate of heat storage in the deep ocean H . Their evolution in the (N, T) space
257 is illustrated in Fig. 1 (third row). The linear term takes into account the fact that the
258 surface temperature is not in equilibrium, which induces a radiative imbalance. The second
259 term is a deviation from this linear radiative flux due to the non linear evolution of the
260 temperature pattern. The magnitude of H reflects the magnitude of this deviation.

261 Initially, $H = 0, T = 0$ and the radiative imbalance is equal to the forcing. In equilibrium,
262 as H is zero, the assumption of linear dependence between the radiative imbalance and the
263 surface temperature remains valid. But during the transient regime, the net radiative flux is
264 affected by the deep-ocean heat uptake. The parameter usually referred to as the effective
265 feedback parameter $\lambda_{eff} = (\mathcal{F} - N)/T$ varies in time (if $\varepsilon \neq 1$) and needs to be distinguished
266 from the equilibrium feedback parameter λ . Instead of λ_{eff} , a transient radiative feedback
267 function λ_t should be considered, with:

$$\lambda_t = \lambda + (\varepsilon - 1)\gamma\frac{T - T_0}{T}. \quad (24)$$

268 The efficacy factor can be determined from gradual perturbation AOGCMs simulations
269 (by neglecting Cdt/dt) but requires prior knowledge of the equilibrium climate sensitivity
270 and feedback parameter (Winton et al. 2010). On the other hand, all the EBM- ε radiative
271 and thermal inertia parameters can be consistently computed from a step-forcing AOGCM
272 experiment (and a control simulation) only, by taking into account the time evolution of the
273 transient radiative feedback function. In the next section, the method used to adjust the
274 EBM- ε physical parameters to a given AOGCM is briefly described.

275 *d. Method for EBM- ε parameter calibration*

276 In comparison with the EBM-1, the EBM- ε has an additional radiative parameter ε
 277 that needs to be tuned consistently with the reference radiative forcing amplitude (e.g.
 278 \mathcal{F}_{2xCO_2} for a $2xCO_2$ perturbation) and the equilibrium feedback parameter λ from the N - T
 279 evolution. The physical parameters of the EBM- ε are computed iteratively using a step-
 280 forcing experiment. The parameters are initially set to the EBM-1 values ($\varepsilon = 1$, and
 281 parameters computed in G12). For each iteration i , the deep-ocean heat uptake $H^{(i-1)}$
 282 is first evaluated using the analytical solutions and the thermal parameters computed at
 283 iteration $(i - 1)$. Then, using Eq. (3), a multi-linear regression of N (AOGCM values)
 284 against the AOGCM surface temperature response T and $H^{(i-1)}$ provides the values of $\mathcal{F}^{(i)}$,
 285 $\lambda^{(i)}$ and $\varepsilon^{(i)}$:

$$N = \mathcal{F}^{(i)} - \lambda^{(i)}T - (\varepsilon^{(i)} - 1)H^{(i-1)}. \quad (25)$$

286 Finally the thermal inertia parameters $C^{(i)}$, $C_0^{\prime(i)}$ and $\gamma^{\prime(i)}$ are tuned by performing two
 287 fits of the surface temperature response following the methodology used for the EBM-1
 288 calibration (see details in Section 3 of G12). Few iterations are found to be sufficient to
 289 obtain convergence. This method for estimating the equilibrium climate sensitivity, radiative
 290 parameters and thermal inertia parameters from a short-term step-forcing simulation will
 291 be referred in the following as the EBM- ε method. In the next section, the EBM- ε method
 292 is applied to 12 CMIP5 AOGCMs using the abrupt $4xCO_2$ experiment, and results are
 293 compared to the EBM-1 estimates (which, for the radiative properties, correspond to the
 294 estimates from Gregory et al. (2004)’s method).

3. Validation for CMIP5 AOGCMs

a. Radiative parameters and TOA net flux, comparison with the EBM-1

For the same twelve AOGCMs of the CMIP5 database analyzed in G12, the EBM- ε method is applied and radiative parameter values are reported in Table 1. The values of deep-ocean heat-uptake efficacy factor are mostly greater than 1 (see also Fig. 4a). Only two models (INM and CNRM) have values of ε smaller than unity. The heat-uptake efficacy factor ranges from 0.83 to 1.82 with a multimodel mean value of 1.29 and an intermodel standard deviation of 0.27. These results are in very good agreement with the estimates of Winton et al. (2010) for some CMIP2 and CMIP3 models analysis despite methodological differences. Winton et al. (2010) derived the ε from 1% y^{-1} CO_2 increase experiments using equilibrium climate sensitivity mainly derived from AGCMs coupled with a mixed-layer ocean model and using forcing estimates taken from Solomon et al. (2007). The latter were computed from different sources and they took into account either only the stratospheric adjustment or both stratospheric and tropospheric adjustments [through the method of Gregory et al. (2004)], depending on cases. In this study, the efficacy factor ε , the radiative forcing and the equilibrium climate sensitivity are derived jointly in the single framework of the EBM- ε .

Figures 2 and 3 compare for each model the N - T plot for AOGCM results, EBM- ε fit, and Gregory et al. (2004)'s linear regression. For models with an efficacy factor near 1 (CNRM, IPSL, MIROC), the assumption of linearity between N and T is valid and the results from EBM- ε are close to that of the linear model. For models with large ε (CSIRO, MOHC, NCC, MPIM), the results from EBM- ε largely improve the fit of radiative imbalance versus temperature response compared to a linear fit. In particular, the EBM- ε is able to reproduce the two-stage behaviour of these models in the parameter space (N , T).

Figures 4b-d compare the values of $\mathcal{F}_{4\times\text{CO}_2}$, λ and $T_{eq4\times\text{CO}_2}$ obtained within the framework of the EBM- ε and those derived with the method described in Gregory et al. (2004). The

321 three AOGCMs with ε larger than 1.5 are indicated in full black markers. For these models,
322 the radiative forcing amplitude and the equilibrium climate sensitivity are larger than in the
323 standard linear model estimate. Indeed for CSIRO and MOHC, the equilibrium temperature
324 response for a $4xCO_2$ perturbation is up to 2 K warmer than the value derived from the
325 linear assumption. The multimodel mean is 0.5 K warmer. The radiative forcing is 1 to
326 2 W m^{-2} larger for large ε models and the multimodel mean is 0.6 W m^{-2} larger. Most
327 models have a forcing lower than 7.5 W m^{-2} except CCCMA, MPIM and MIROC. The
328 two latter have a forcing of the order of 9 W m^{-2} , which suggests a strong effect of the
329 tropospheric adjustment. The change in the ECS is mainly due to a change in the forcing,
330 the radiative feedback parameters being less impacted. Moreover, contrary to the forcing
331 and the equilibrium temperature, the sign of the λ difference between the EBM-1 and the
332 EBM- ε estimates is independent of the sign of $\varepsilon-1$. For example, for MOHC and CSIRO,
333 λ is respectively larger and lower with the EBM- ε method whereas both have an ε value
334 greater than 1. The multimodel radiative forcing and radiative feedback parameter standard
335 deviations are roughly unchanged whereas the equilibrium temperature one increases from
336 1.6 to 2.1 K. The improved match of the temperature response and radiative imbalance
337 evolution between the AOGCMs and the simple EBM suggests that the values estimated
338 from the EBM- ε method are more accurate. However, a complete assessment of the EBM- ε
339 would require to extend AOGCM experiments until equilibrium, i.e., over a period of 1000
340 to 1500 years.

341 *b. Thermal inertia parameters and temperature, comparison with the EBM-1*

342 The thermal inertia physical parameters and the relaxation times are given in Table 2 and
343 represented as a function of their EBM-1 counterparts in Figs. 4e-i. The fast relaxation time
344 scale τ_f is not impacted by the inclusion of the efficacy of deep-ocean heat uptake whereas
345 the slow relaxation timescale τ_s is. The change in τ_s is mainly due to change in the heat
346 exchange coefficient γ rather than in the deep-ocean surfacic heat capacity C_0 . Models with

347 $\varepsilon > 1$ have a lower γ than in the EBM-1 framework. The inclusion of the effect represented
348 by the deviation term $(1 - \varepsilon)H$ upon the temperature response amounts to modifying the
349 deep-ocean heat uptake such that the heat exchange coefficient is $\varepsilon\gamma$. The lack of efficacy
350 factor in the EBM-1 is compensated by a large γ when $\varepsilon > 1$.

351 The EBM-1 also underestimates the upper-ocean surfacic heat capacity C . The estimate
352 of C depends on the forcing estimation since it is evaluated through an estimation of the
353 temperature tendency at $t=0$ that is equal to \mathcal{F}/C . Consequently, an underestimation of
354 \mathcal{F} leads to an underestimation of C . These results suggest that the lack of radiative effect
355 associated with deep-ocean heat uptake introduces a bias in the EBM-1 estimates of the
356 thermal inertia parameters. The standard deviation of γ , C_0 and C is reduced with the
357 EBM- ε , respectively from 0.13 to 0.11 $\text{W m}^{-2} \text{K}^{-1}$, 71 to 58 $\text{W y m}^{-2} \text{K}^{-1}$ (but slightly
358 increased from 26 to 29 $\text{W y m}^{-2} \text{K}^{-1}$ if the INM is excluded) and 0.8 to 0.6 W y m^{-2}
359 K^{-1} . This shows that introducing a new degree of freedom reduces slightly the inter-model
360 spread.

361 Figure 5 shows the temperature response of the three AOGCMs with the largest ε esti-
362 mates (CSIRO, NCC, and MOHC) for the abrupt $4x\text{CO}_2$ and the $1\% \text{ y}^{-1} \text{CO}_2$ experiments,
363 as well as the EBM-1 and the EBM- ε analytical solutions using the parameters estimated
364 by the corresponding method on the basis of the abrupt $4x\text{CO}_2$ experiment. The tempera-
365 ture responses are identical for both EBMs in both the abrupt $4x\text{CO}_2$ and the $1\% \text{ y}^{-1} \text{CO}_2$
366 simulations over the first 150 years, and they match the AOGCM responses. But, for the
367 step-forcing scenario, the EBM- ε response diverges from the EBM-1 response after about
368 300 years. Only the second phase of the temperature evolution, the one driven by the slow
369 component of the system, is modified by the introduction of an efficacy factor. This is con-
370 sistent with the fact that only the slow relaxation timescale varies between the EBM-1 and
371 the EBM- ε methods. The EBM-1 calibrated with the abrupt simulation is accurate enough
372 to represent the temperature evolution over the centennial scale. However, compared to
373 the EBM- ε estimates, the EBM-1 parameters are biased as a result of a bias in radiative

374 parameters estimated following the method of Gregory et al. (2004).

375 *c. Parameters dependency*

376 In this section, the question of potential relationships between the EBM- ε parameters is
377 investigated. Table 3 shows the multimodel correlations between parameters of the EBM- ε ,
378 and also between these parameters and the equilibrium temperature response. For the set of
379 12 models, a correlation coefficient higher than 0.58 is significant at the 95% confidence level.
380 As expected, the anticorrelation between T_{eq} and λ is high, with a correlation coefficient of
381 -0.86. No correlation is found between \mathcal{F} and λ suggesting that the effect of fast tropospheric
382 adjustment is independent of the surface temperature feedback. Consistently, the equilibrium
383 temperature is independent of the adjusted forcing magnitude.

384 Raper et al. (2002) suggested a negative correlation between their heat exchange coeffi-
385 cient κ of the one-box model (that is similar to the parameter γ) and the radiative feedback
386 parameter λ but Gregory and Forster (2008) and Plattner et al. (2008)'s analysis of CMIP3
387 models did not find such a correlation. Including an interactive deep ocean changes the
388 formulation of deep-ocean heat uptake and impacts the relationship between the heat ex-
389 change coefficient (κ or γ) and the radiative feedback parameter λ . Indeed, the EBM- ε
390 estimates of λ and γ are positively correlated, with a correlation coefficient of 0.42 that is
391 too small to be significant. The correlation between the corresponding EBM-1 estimates is
392 even weaker (0.13). These results support Gregory and Forster (2008) and Plattner et al.
393 (2008)'s conclusions.

394 All but two of the correlation coefficients between parameter estimates are found to be
395 insignificant. Note that if the INM, which is somewhat of an outlier (see G12) is excluded,
396 the correlations between parameters are even weaker, and further from the significant level.
397 The equilibrium temperature and ε are significantly correlated, with a correlation coefficient
398 of 0.64. The reasons for this are unclear. It is possible that models with a higher climate
399 sensitivity are also models with a higher regional radiative feedback in the region where the

400 warming is slower (which corresponds to a larger ε). Local radiative feedbacks and horizontal
 401 heat transports would need to be investigated in order to answer this question.

402 The heat exchange coefficient γ and the surfacic heat capacity C are significantly corre-
 403 lated with a correlation coefficient of 0.62. Models with a higher upper-ocean heat capacity
 404 are also models that allow a larger heat flux between the upper ocean and the deep ocean
 405 for a smaller temperature difference between the two layers. More heat is accumulated in
 406 the upper ocean and also more heat is transported to the deep ocean for a given surface
 407 temperature. This might be an artefact of the oversimplified modeling of heat uptake in the
 408 two-box model, or it might result from energy constraints on the heat uptakes: for given heat
 409 uptakes, a large C yields a small temperature response T , which has to be compensated by
 410 a large γ in order to maintain upper-to-deep oceanic heat flux (that equals the deep-ocean
 411 heat uptake).

412 *d. Decomposition in longwave and shortwave contributions*

413 In this section, the net TOA radiative flux is decomposed in longwave (LW) and shortwave
 414 (SW) components, respectively N^{LW} and N^{SW} . We introduce LW and SW radiative feedback
 415 parameters associated to the deep-ocean heat-uptake temperature, respectively λ_D^{LW} and λ_D^{SW}
 416 and we assume the decomposition in an upper-ocean and a deep-ocean radiative contribution
 417 is valid for each component separately. These assumptions yield the following equations:

$$N^{LW} = \mathcal{F}^{LW} - \lambda^{LW}T - (\lambda^{LW} - \lambda_D^{LW})\frac{\varepsilon}{\lambda}H, \quad (26)$$

$$N^{SW} = \mathcal{F}^{SW} - \lambda^{SW}T - (\lambda^{SW} - \lambda_D^{SW})\frac{\varepsilon}{\lambda}H, \quad (27)$$

418 where \mathcal{F}^{LW} , \mathcal{F}^{SW} , λ^{LW} and λ^{SW} are, respectively, the LW and the SW components of the
 419 radiative forcing and of the radiative feedback parameter. Unlike in the case of the total
 420 feedback, we do not define a SW or LW efficacy factor ε_{SW} or ε_{LW} . Indeed, although the
 421 total feedback is necessary different from zero, it is possible that λ^{SW} (λ_D^{SW}) is zero whereas
 422 λ_D^{SW} (λ^{SW}) is not. In such a case, a shortwave efficacy factor ε_{SW} would have no sense.

423 Each LW and SW component is calculated by multi-linear regression of the corresponding
424 net radiation flux as a function of temperature (both from the AOGCM abrupt 4xCO₂
425 experiment) and $\frac{\varepsilon}{\lambda}H$ (from the EBM- ε estimation). Values of the tuned LW and SW radiative
426 parameters are reported in Table 4 and resulting fits for each model separately shown in
427 Figs. 6 and 7. These figures reflect the large intermodel spread in both forcing and radiative
428 feedback parameters LW and SW components.

429 AOGCMs that have a large SW forcing contribution can have a large LW contribution
430 (MPIM) or a small LW contribution (IPSL). The 4xCO₂ LW forcing ranges from 3.4 to 7.4
431 W m⁻² with an ensemble mean of 6.1 W m⁻² and a standard deviation of 1.1 W m⁻². The
432 4xCO₂ SW forcing is mostly positive with a mean value of 1.3 W m⁻² except for two models
433 (CSIRO, INM). Its standard deviation is slightly larger than the one of the LW contribution.
434 By comparison with estimates taking into account the stratospheric adjustment only, the
435 forcing is found to be lower in the LW and larger in the SW. Indeed, Forster and Taylor (2006)
436 found a forcing estimate of 3.45 W m⁻² in the LW for a 2xCO₂ experiment (corresponding
437 to 6.90 W m⁻² for a 4xCO₂ experiment). The instantaneous SW forcing is of the order
438 of -0.06 W m⁻² (Myhre et al. 1998). These estimates confirm Gregory and Webb (2008)
439 and suggest a non negligible effect of the fast change in the cloud component (among the
440 other feedbacks) on the radiative forcing adjustment. However, the LW and SW forcings
441 are larger than Gregory and Webb (2008)'s estimates (respectively 2.84 and 0.50 W m⁻²
442 for an ensemble of 2xCO₂ experiments) which is consistent with $\varepsilon > 1$ for most models.
443 Thus, for the majority of AOGCMs, the EBM- ε estimation decreases the LW contribution
444 of the tropospheric adjustment and increases the SW contribution in comparison with an
445 estimation based on a linear fit.

446 The LW contribution to the feedback parameter λ^{LW} is positive (i.e. negative feedback)
447 for all models because the radiative imbalance is restored by increased LW emission associ-
448 ated with the temperature increase. The SW contribution to the feedback parameter λ^{SW}
449 is negative (i.e. positive feedback) for all models except GFDL which has a negligible λ^{SW} .

450 For most AOGCMs, λ^{SW} is above (in absolute value) the 0.2-0.4 W m⁻² K⁻¹ typical range
451 of the albedo feedback, suggesting a positive feedback of clouds in the SW.

452 The deep-ocean heat-uptake feedback parameter λ_D^{LW} is generally of the same order of
453 magnitude as λ^{LW} but λ_D^{SW} is smaller than λ^{SW} . This suggests that the value of $\varepsilon > 1$
454 obtained for the majority of the models is mainly due to the shortwave radiation, with low
455 clouds as a good candidate to explain most of the difference between EBM- ε and EBM-
456 1. Further analysis is necessary to understand which components of the climate system
457 are responsible for the differences and quantify each contribution. But the results of such a
458 simple SW-LW decomposition suggest that the EBM- ε framework can be used to decompose
459 the radiative fluxes such as a cloud/clear-sky decomposition or more complex decompositions
460 such as partial radiative fluxes.

461 4. Conclusion

462 In this study, the two-box energy-balance model with an efficacy factor of deep-ocean heat
463 uptake is used as a tool to estimate the first-order global thermal properties of AOGCMs.
464 These thermal properties include both radiative properties and thermal inertia properties. It
465 is shown that the temperature response can be decomposed as the balanced response to three
466 "forcings": the TOA radiative forcing, the upper-ocean heat uptake and the deep-ocean heat
467 uptake. Assuming additivity of each temperature response patterns to these "forcings" and
468 assuming the separability of time and spatial variability of these temperature responses, the
469 radiative feedback parameter associated with the deep-ocean heat uptake is shown to be
470 different from the equilibrium feedback parameter, seeing that the local feedback parameter
471 varies geographically. This results in the presence of an additional term in the radiative
472 imbalance formulation depending on the deep-ocean heat uptake.

473 Within this EBM- ε framework, the concepts of effective forcing and effective climate
474 sensitivity are unchanged but the concept of effective feedback parameter is modified. The

475 effective forcing remains the physical parameter defined by Gregory et al. (2004), i.e., the
476 value of the net radiative imbalance when the temperature tends to zero. It is sensitive
477 to fast feedbacks due to changes in both stratospheric and tropospheric variables, such as
478 clouds, temperature lapse rate, and water vapour amount, associated with the external
479 radiative perturbation, but unassociated with the surface temperature response. However,
480 the effective climate feedback parameter such as usually defined, i.e., the feedback parameter
481 of the transient regime, needs to be distinguished from the equilibrium feedback parameter.
482 The effective equilibrium feedback parameter is assumed to be constant for a given type of
483 forcing agent, a given spatial distribution of the forcing amplitude but it is valid only for
484 an equilibrium state. The transient feedback function involves an additional term that can
485 depend on deep-ocean heat uptake and it can thus vary in time.

486 An iterative method of calibration is proposed and applied to twelve CMIP5 AOGCMs.
487 The results show that the model reproduces with accuracy the evolution of the radiative
488 imbalance as a function of the temperature response during a transient regime. The fits
489 of the temperature evolution over the time of simulation (about 150 years) are the same as
490 those obtained with the EBM-1. However, the physical parameters of the model are different.
491 The improved match of the temperature response and radiative imbalance evolution between
492 the AOGCMs and the EBM suggests that the values estimated from the EBM- ε method are
493 more accurate. Moreover, the method is applied to the LW and the SW component of the
494 radiative flux. Each evolution separately is well represented suggesting that the method can
495 be applied to partial decomposition of the radiative imbalance.

496 The benefit of two-box EBMs such as the EBM-1 and EBM- ε is that they are the simplest
497 EBMs that represent both the beginning of the simulation (determined by the forcing) and
498 the end of the experiment (determined by the equilibrium climate sensitivity for a constant
499 forcing). One-box EBMs are unable to represent both phases of the time evolution. The
500 advantage of the EBM- ε on the EBM-1 is that the net TOA imbalance is better represented as
501 a function of the global surface temperature response. The EBM- ε can be used to compute

502 the radiative parameters and the effective climate sensitivity consistently from one single
503 methodology and one single short AOGCM experiment, by taking into account the time
504 variation of the effective feedback function. From this point of view, the calibration of the
505 EBM- ε method constitutes a new, improved method to determine the climate sensitivity
506 and the adjusted forcing of an AOGCM.

507 Such two-box EBM offers a complete first-order explanation of the behaviour of climate
508 models under an externally imposed perturbation. The spread on the radiative and thermal-
509 inertia global parameters within a generation of models (such as the CMIP5 generation) can
510 be used as a indication of the uncertainty of the multi-model climate projections performed
511 for the Intergovernmental Panel on Climate Change. The evolution of this spread from one
512 CMIP exercise to the next indicates whether AOGCMs converge in terms of global properties.
513 It can also be used for AOGCM's analysis, by relating some of the EBM parameters to
514 physical processes or physical variables that can be directly calculated in the AOGCM. In
515 parallel, the calibration of such model, that could be extended to other type of radiative
516 perturbations, offers a physically-based simple climate model able to emulate the AOGCM
517 response to different idealized scenarios.

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TABLE 1. The $4xCO_2$ radiative forcing \mathcal{F}_{4xCO_2} , total feedback parameter λ , efficacy factor for deep-ocean heat uptake ε , and $4xCO_2$ equilibrium temperature T_{4xCO_2} estimates in the framework of the EBM- ε of the twelve CMIP5 models used in this paper, and their multimodel mean and standard deviation.

Model	\mathcal{F}_{4xCO_2} (W m ⁻²)	λ (W m ⁻² K ⁻¹)	ε	T_{4xCO_2} (K)
BCC (BCC-CSM1-1)	7.4	1.28	1.27	5.8
CCCMA (CanESM2)	8.2	1.06	1.28	7.8
CNRM (CNRM-CM5.1)	7.1	1.12	0.92	6.4
CSIRO (CSIRO-Mk3-6-0)	7.0	0.68	1.82	10.2
GFDL (GFDL-ESM2M)	7.1	1.38	1.21	5.1
INM (INMCM4)	6.0	1.56	0.83	3.9
IPSL (IPSL-CM5A-LR)	6.7	0.79	1.14	8.5
MIROC (MIROC5)	8.9	1.58	1.19	5.6
MOHC (HadGEM2-ES)	6.8	0.61	1.54	11.1
MPIM (MPI-ESM-LR)	9.4	1.21	1.42	7.8
MRI (MRI-CGCM3)	7.1	1.31	1.25	5.4
NCC (NorESM1-M)	7.4	1.15	1.57	6.5
Multimodel mean	7.4	1.14	1.29	7.0
Standard deviation	1.0	0.32	0.27	2.1

TABLE 2. The atmosphere/land/upper ocean surfacic heat capacity C , deep-ocean surfacic heat capacity C_0 , heat exchange coefficient γ and fast and slow relaxation times estimates in the framework of the EBM- ε of the twelve CMIP5 models used in this paper, and their multimodel mean and standard deviation.

Model	C (W y m ⁻² K ⁻¹)	C_0 (W y m ⁻² K ⁻¹)	γ (W m ⁻² K ⁻¹)	τ_f (y)	τ_s (y)
BCC (BCC-CSM1-1)	8.4	56	0.59	4.1	152
CCCMA (CanESM2)	8.0	77	0.54	4.5	139
CNRM (CNRM-CM5.1)	8.3	95	0.51	5.2	266
CSIRO (CSIRO-Mk3-6-0)	8.5	76	0.71	4.2	316
GFDL (GFDL-ESM2M)	8.8	112	0.85	3.6	233
INM (INMCM4)	8.5	271	0.67	4.0	546
IPSL (IPSL-CM5A-LR)	8.1	100	0.57	5.5	327
MIROC (MIROC5)	8.7	158	0.73	3.6	338
MOHC (HadGEM2-ES)	7.5	98	0.49	5.4	457
MPIM (MPI-ESM-LR)	8.5	78	0.62	4.0	220
MRI (MRI-CGCM3)	9.3	68	0.59	4.4	181
NCC (NorESM1-M)	9.7	121	0.76	4.1	328
Multimodel mean	8.5	109	0.64	4.4	300
Standard deviation	0.6	58	0.11	0.7	113

TABLE 3. Intermodel correlations between the equilibrium temperature at 4xCO₂ T_{4xCO_2} and the physical parameters \mathcal{F} , λ , ε , γ , C_0 , C of the EBM- ε for the 12 CMIP5 AOGCMs.

	T_{4xCO_2}	\mathcal{F}	λ	ε	γ	C_0	C
T_{4xCO_2}	1	0.02	-0.86	0.64	-0.38	-0.45	-0.51
\mathcal{F}		1	0.23	0.18	0.06	-0.28	0.12
λ			1	-0.55	0.42	0.46	0.47
ε				1	0.14	-0.48	0.09
γ					1	0.29	0.62
C_0						1	0.06
C							1

TABLE 4. The LW and SW components of the radiative forcing, \mathcal{F}^{LW} and \mathcal{F}^{SW} , of the total feedback parameter, λ^{LW} and λ^{SW} , and of the deep-ocean heat-uptake feedback parameter, λ_D^{LW} and λ_D^{SW} , estimates in the framework of the EBM- ε of the twelve CMIP5 models used in this paper, and their multimodel mean and standard deviation STDV.

Model	\mathcal{F}^{LW} (W m ⁻²)	\mathcal{F}^{SW} (W m ⁻²)	λ^{LW} (Wm ⁻² K ⁻¹)	λ^{SW} (Wm ⁻² K ⁻¹)	λ_D^{LW} (Wm ⁻² K ⁻¹)	λ_D^{SW} (Wm ⁻² K ⁻¹)
BCC	6.4	1.0	1.69	-0.42	1.68	-0.68
CCCMA	6.2	2.0	1.42	-0.37	1.38	-0.57
CNRM	5.1	2.1	1.62	-0.50	1.67	-0.46
CSIRO	7.4	-0.4	1.97	-1.29	1.81	-1.43
GFDL	5.4	1.7	1.37	0.01	1.68	-0.54
INM	6.8	-0.7	2.12	-0.55	2.65	-0.76
IPSL	3.4	3.3	1.92	-1.13	1.89	-1.20
MIROC	6.9	2.0	1.93	-0.35	1.70	-0.37
MOHC	6.2	0.6	1.56	-0.96	1.55	-1.16
MPIM	7.0	2.5	1.67	-0.46	1.50	-0.65
MRI	6.6	0.5	2.24	-0.93	2.16	-1.11
NCC	6.3	1.1	1.82	-0.67	1.67	-0.93
Mean	6.1	1.3	1.78	-0.63	1.78	-0.82
STDV	1.1	1.2	0.27	0.37	0.34	0.34

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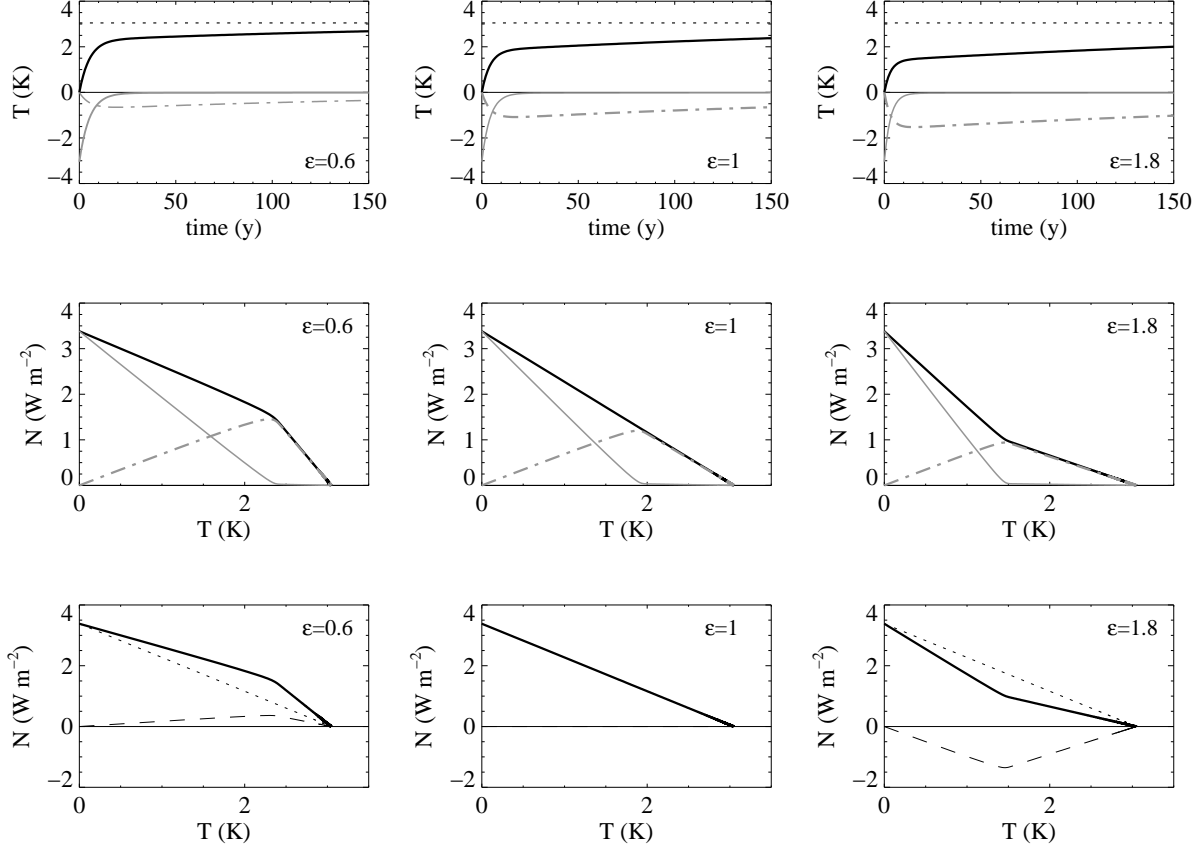


FIG. 1. EBM- ε results. Upper panels: time evolution of global mean surface air temperature (thick black), upper-ocean heat-uptake temperature T_U (thick grey) and deep-ocean heat-uptake temperature T_D (dot-dashed grey) for a step-forcing case; the black dotted line shows the equilibrium temperature T_{eq} . Middle panels: global mean net radiative flux (thick black) and its decomposition into $N_U = -\lambda T_U$ (thick grey) and $N_D = -\lambda_D T_D$ (dot-dashed grey) as functions of the global mean surface air temperature. Bottom panels: global mean net radiative flux (thick black, same as above) and its decomposition into the linear term $\mathcal{F} - \lambda T$ (dot grey) and the deviation term $-(\varepsilon - 1)H$ (dashed grey). Plots are for three ε values indicated on the panels and $\mathcal{F} = 3.9 \text{ W m}^{-2}$, $\lambda = 1.3 \text{ W m}^{-2} \text{ K}^{-1}$, $C = 8 \text{ W y m}^{-2} \text{ K}^{-1}$, $C_0 = 100 \text{ W y m}^{-2} \text{ K}^{-1}$, $\gamma = 0.7 \text{ W m}^{-2} \text{ K}^{-1}$.

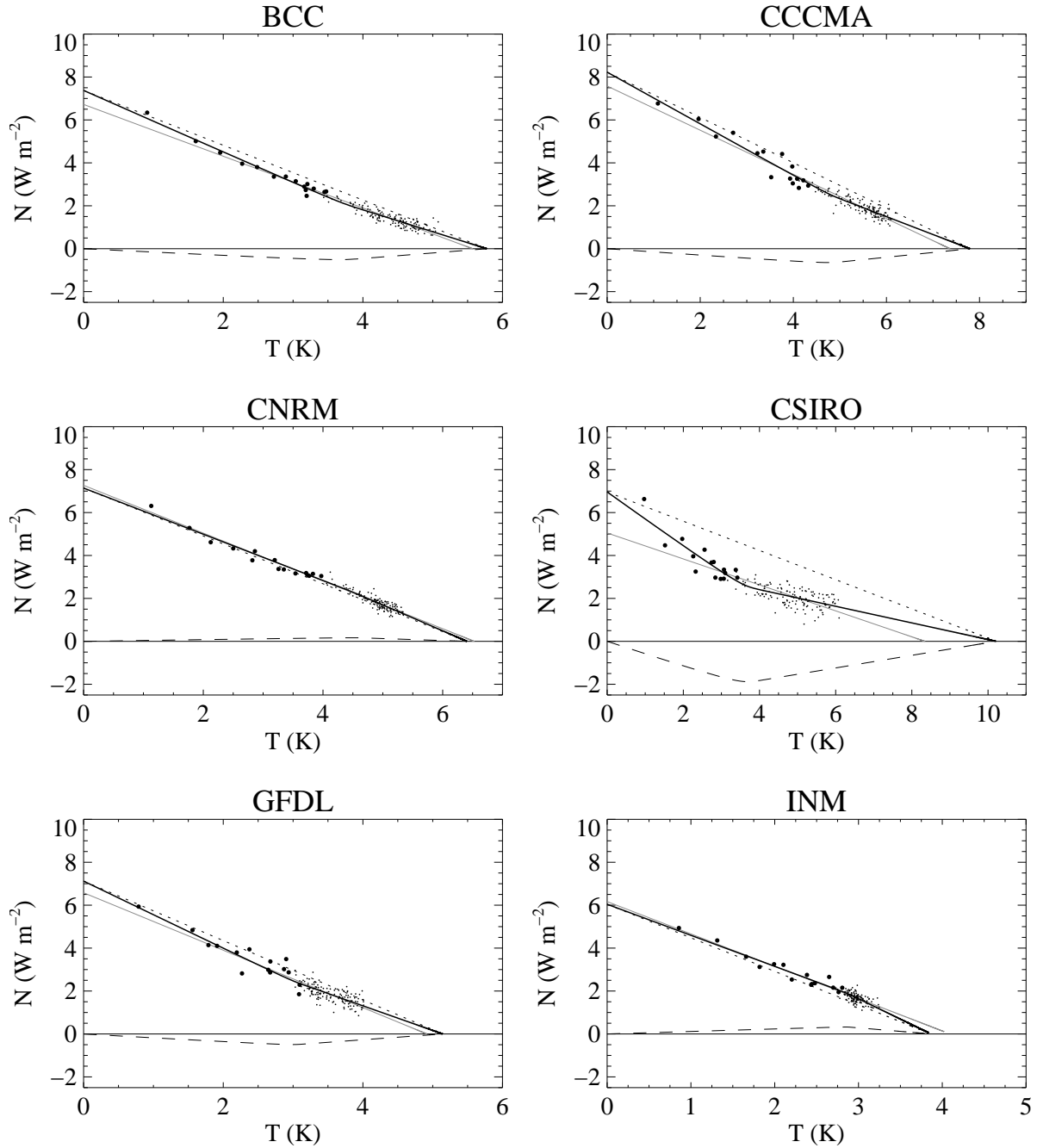


FIG. 2. Global mean net radiative flux at TOA N as a function of global mean surface air temperature T for the abrupt $4\times\text{CO}_2$ experiments (black dots, large dots for the first 15 years), for 6 AOGCMs. The thick black line is the EBM- ϵ fit. The dotted and dashed lines show, respectively, the linear contribution $\mathcal{F} - \lambda T$ and the deviation contribution $-(\epsilon - 1)H$. The grey line is Gregory et al. (2004)'s linear fit. The thin black line shows $N = 0$. Note that the range of T can differ from one panel to another.

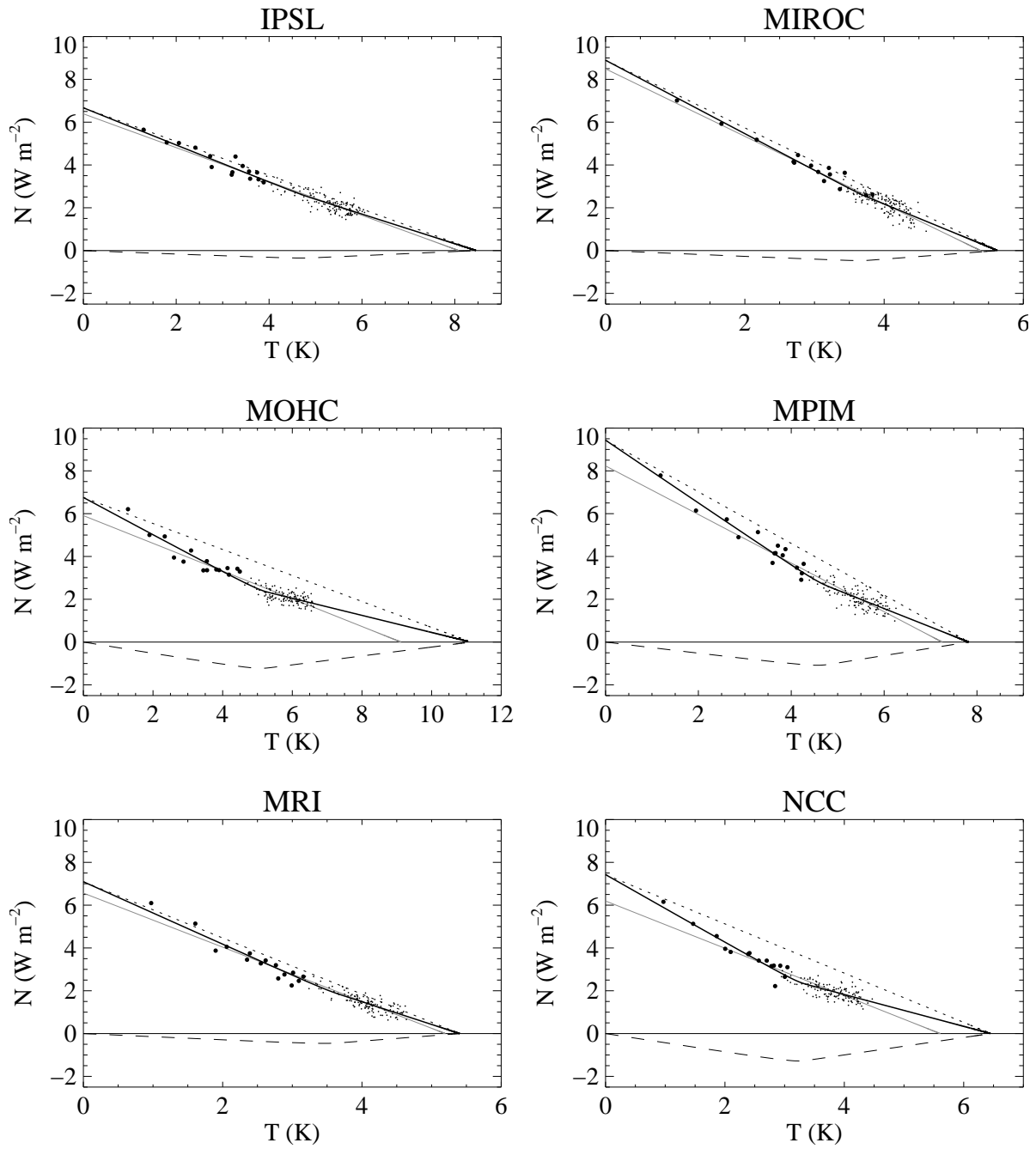


FIG. 3. Same as Fig. 2 for the 6 other AOGCMs.

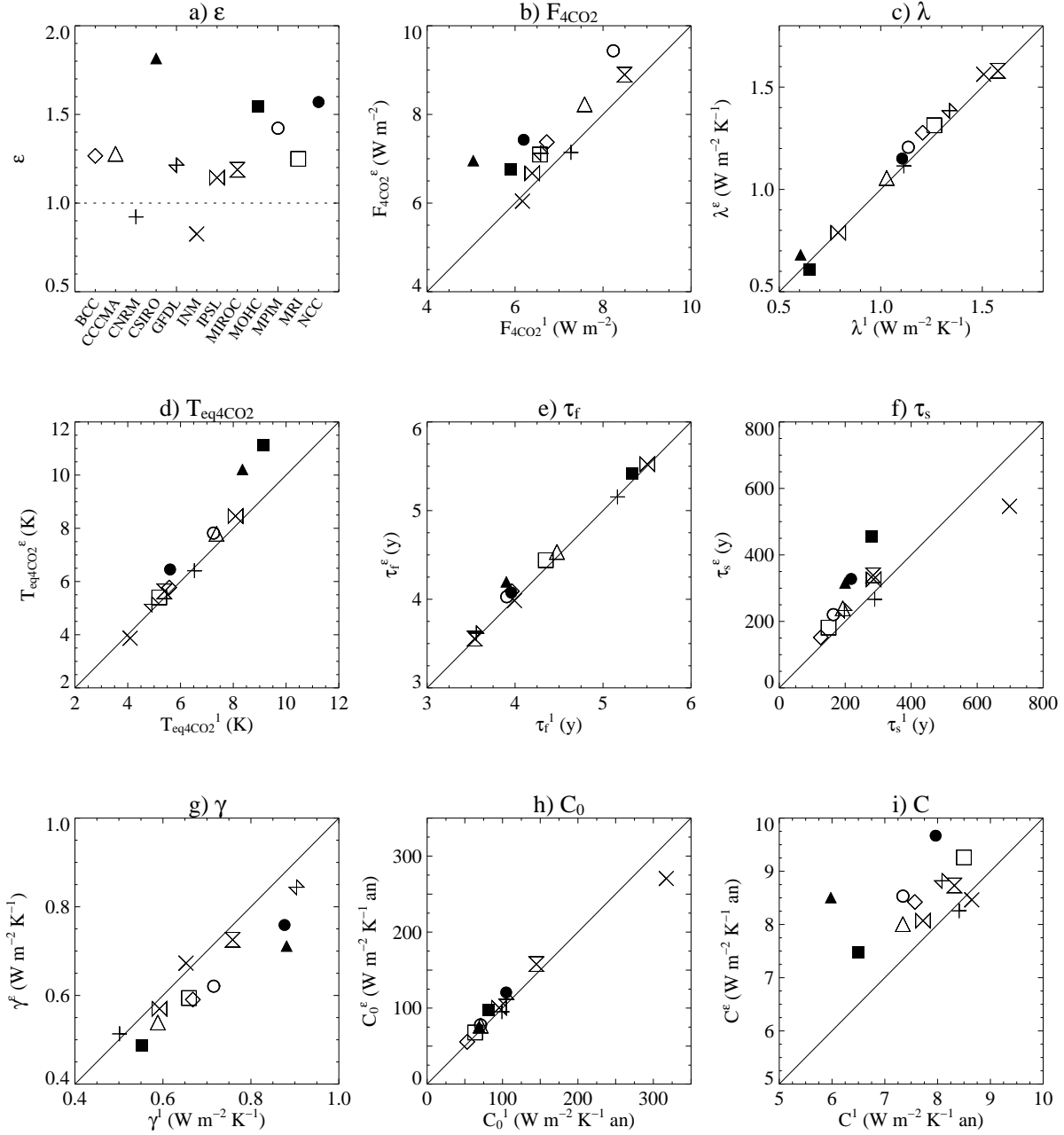


FIG. 4. Parameter estimates: ε values for the 12 AOGCMs (a) and EBM- ε estimates as a function of EBM-1 estimates for \mathcal{F}_{4xCO_2} (b), λ (c), T_{eq4xCO_2} (d), τ_f (e), τ_s (f), γ (g), C_0 (h), and C (i). Superscripts 1 and ε denote, respectively, estimates from the EBM-1 and the EBM- ε methods. The dotted line shows $\varepsilon = 1$ in (a), and the solid lines in (b)-(i) indicate a perfect match between EBM- ε and EBM-1 estimates.

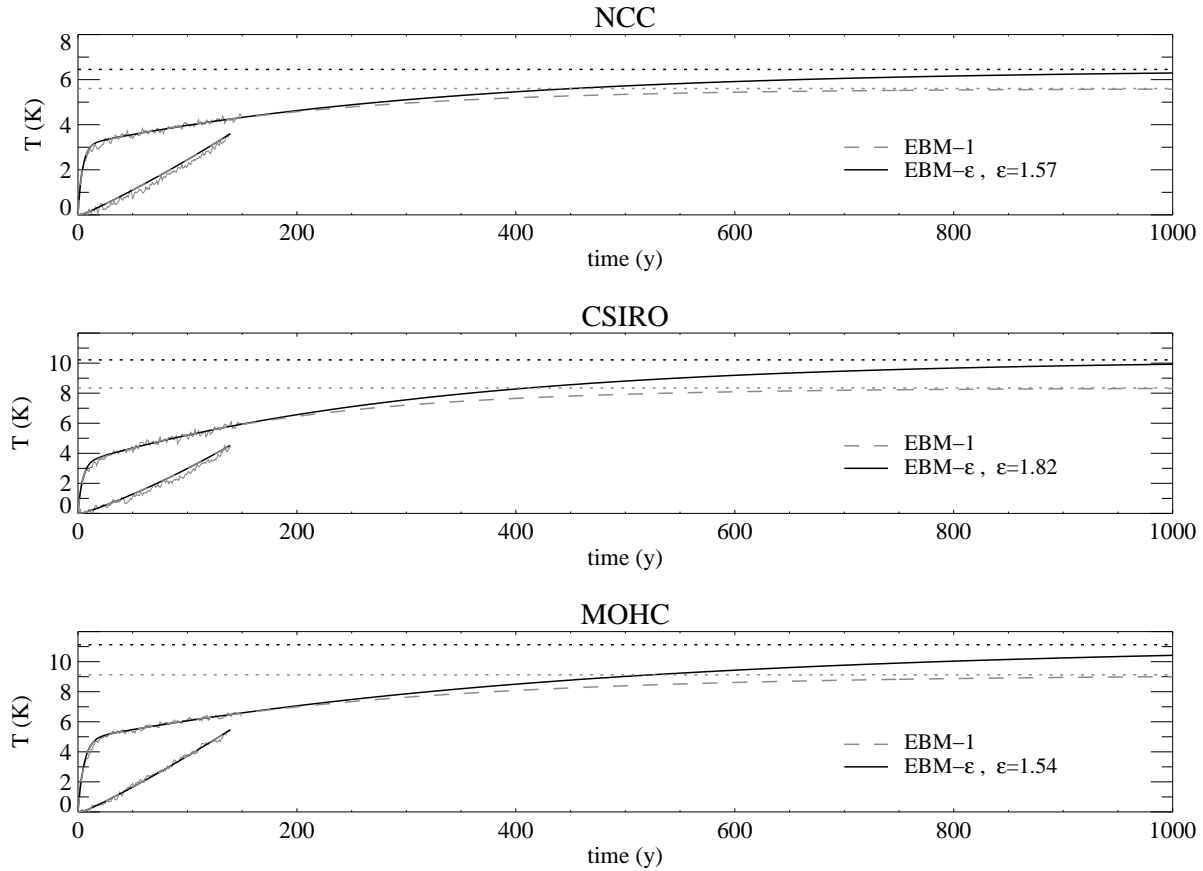


FIG. 5. Temperature response of AOGCMs with the highest ϵ value for the abrupt $4xCO_2$ and $1\% y^{-1} CO_2$ experiments (grey dots) and corresponding fit for EBM-1 (dashed grey) and EBM- ϵ (thin black). Note that the EBM-1 and the EBM- ϵ solutions are superposed for the $1\% y^{-1} CO_2$ and the beginning of the abrupt $4xCO_2$ experiments. The dotted lines denote the equilibrium temperature for EBM-1 (grey) and EBM- ϵ (black).

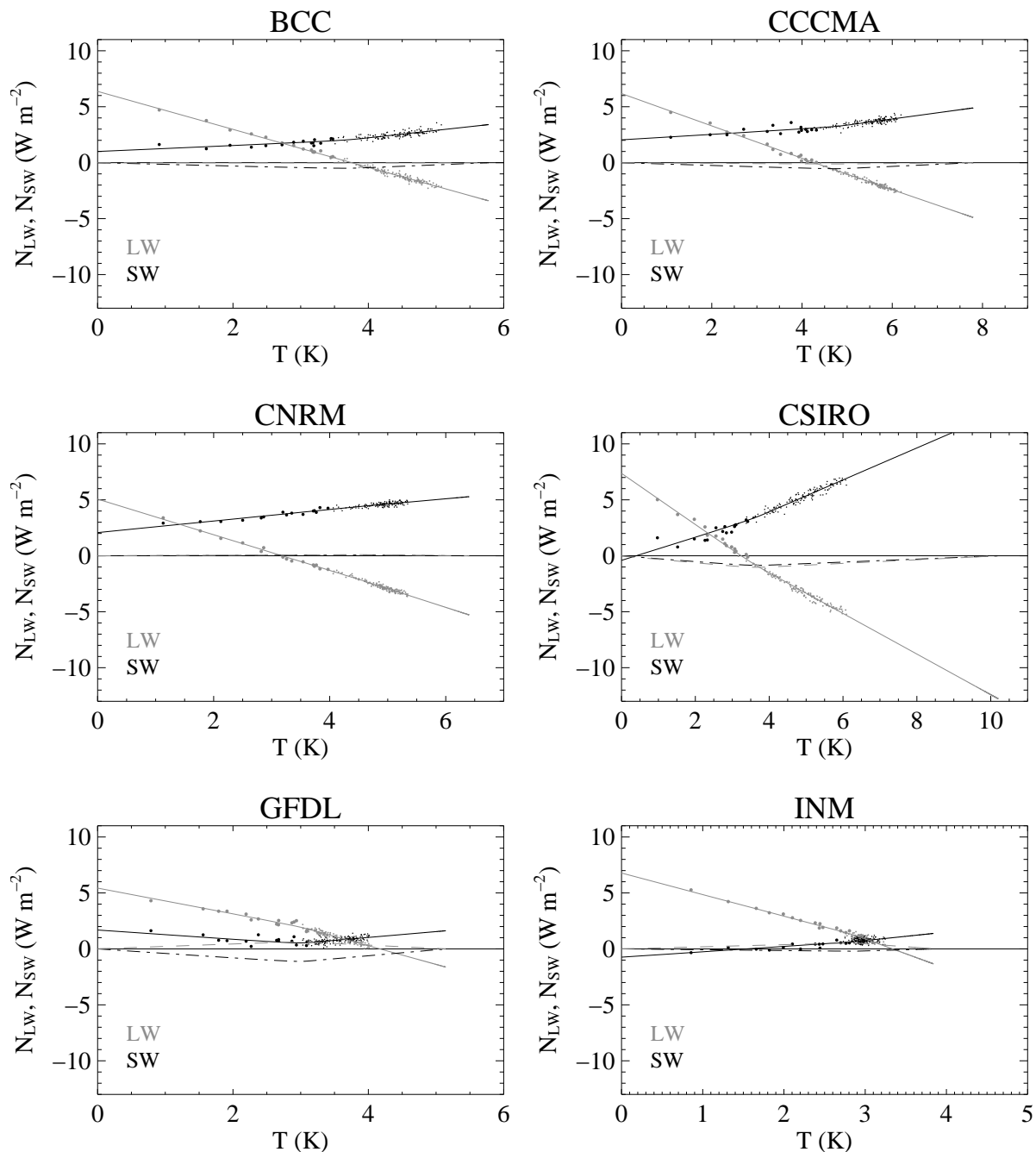


FIG. 6. Global mean net LW (grey) and SW (black) radiative flux at TOA as a function of global mean surface air temperature T for the abrupt $4\times\text{CO}_2$ experiments (black dots, large dots for the first 15 years), for the first 6 AOGCMs. The thick grey and black lines are the EBM- ϵ fits, respectively of the LW and the SW radiative flux. The grey dashed line and the black dot-dashed lines show, respectively, the LW and SW components of the $-(\epsilon - 1)H$ term. The thin black line shows $N = 0$. Note that the range of T can differ from one panel to another.

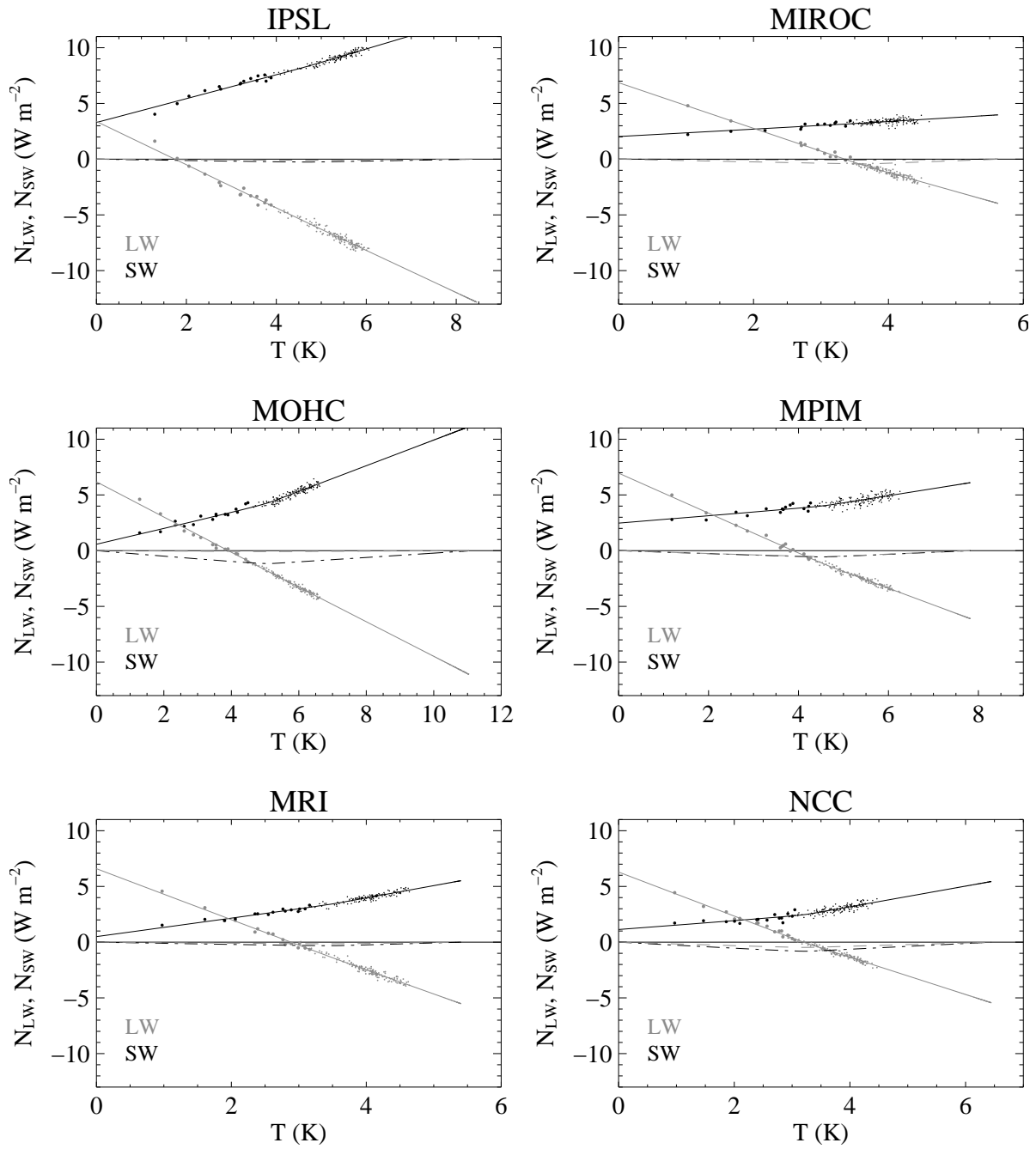


FIG. 7. Same as Fig. 6 for the 6 other AOGCMs.